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Rational design of anti-freezing electrolytes for extremely low-temperature aqueous batteries

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Designing anti-freezing electrolytes through choosing suitable H₂O-solute systems is crucial for low-temperature aqueous batteries (LTABs). However, the lack of an effective guideline for choosing H₂O-solute systems based on decisive temperature-limiting factors hinders the development of LTABs. Here we identified two decisive factors: thermodynamic eutectic temperature (T_e) and kinetic glass-transition temperature (T_{a}) , with T_{a} being applicable for LTABs only when H₂O-solute systems have strong super-cooling ability. We proposed a general strategy wherein low-T_e and strong-super-cooling ability electrolytes can be realized by creating multiple-solute systems via introducing assisted salts with high ionic-potential cations (for example, Al³⁺, Ca²⁺) or cosolvents with high donor numbers (for example, ethylene glycol). As a demonstration in Na-based systems, we designed electrolytes with ultralow T_e (-53.5 to -72.6 °C) and T_{σ} (-86.1 to -117.1 °C), showcasing battery performances including 80 Wh kg⁻¹ and 5,000 cycles at 25 °C, and 12.5 Wh kg⁻¹ at -85 °C. The work provides effective guidelines for the design of anti-freezing electrolytes for extremely low-temperature applications.

With the increasing demand for applications under extremely low-temperature conditions, such as those found in extreme climates, outer space and deep sea environments¹⁻⁵, extensive attention has been paid to the design of anti-freezing electrolytes for rechargeable batteries, particularly aqueous batteries, as the water is prone to freezing⁶⁻⁹. According to typical equilibrium and non-equilibrium H_2O -solute phase diagrams⁶, the freezing temperatures of H_2O -solute systems involve three important terms for low-temperature applications: freezing point (T_f), eutectic temperature (T_e) and glass-transition temperature (T_g). The different roles and effects of T_f , T_e and T_g on low-temperature batteries are often overlooked in designing anti-freezing electrolytes, which hinders the development of extreme LTABs.

First, most researchers have focused on regulating electrolyte $T_{\rm f}$ via various approaches^{10–15}. However, $T_{\rm f}$ is not the most important temperature-limiting factor for low-temperature batteries. For instance, the partially frozen Li⁺, Na⁺, K⁺, Zn²⁺, H⁺ and/or Cl⁻-based^{16–21}

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Fig. 1|Schematic evolution of a dilute solution in the H_2O -solute system during cooling process and the difference between traditional and our proposed strategies. The freezing process involves several typical temperature terms of H_2O transitioning to ice (T_f), H_2O transitioning to the mixture of ice and water of crystallization (T_e), H_2O transitioning to glassy water (T_g).

aqueous electrolytes enable batteries to operate at temperatures below their $T_{\rm f}$. According to a typical equilibrium H₂O-solute phase diagram⁶, the $T_{\rm e}$ rather than the $T_{\rm f}$ is the thermodynamic decisive temperature-limiting factor for battery operation. As shown in Fig. 1, the $T_{\rm f}$ is the temperature at which an electrolyte begins to freeze and is in a partially frozen state, whereas the T_e is the temperature at which an electrolyte totally freezes. In a given H₂O-solute system⁶, electrolytes with varying concentrations usually have different $T_{\rm f}$, but they would have the same T_e . The T_f is usually not lower than the T_e ($T_f \ge T_e$; T_f equals T_e only when electrolyte concentration is the same as the eutectic-point concentration in equilibrium H₂O-solute phase diagram⁶). At temperatures below $T_{\rm f}$, a dilute electrolyte usually becomes a mixture of ice and concentrated electrolyte (Fig. 1), and the mixture could still remain at a high enough ionic conductivity owing to the connected liquid region¹⁷ before it is totally frozen as the crystalline state at Te. Therefore, it is crucial to design anti-freezing electrolytes by choosing low- T_e H₂O-solute systems for extremely low-temperature applications.

Second, some anti-freezing electrolytes²² exhibit ultralow T_{g} heat-flow steps on the differential scanning calorimetry (DSC) curves. However, T_{α} is a kinetic decisive temperature-limiting factor for low-temperature batteries and is only applicable for H₂O-solute systems with strong super-cooling ability (SCA). For instance, the 7 mol kg⁻¹ (m) LiCl electrolytes have a $T_{\rm f}$ of -58 °C and a $T_{\rm e}$ of -74 °C according to the equilibrium H_2O -LiCl phase diagram²³, but it was reported to enable aqueous battery operation at -78 °C (ref. 20). This should be attributed to the strong SCA of H₂O-LiCl system. The concentrated solution in the H₂O-LiCl system can maintain a super-cooling liquid state at temperatures between its T_e (-74 °C)²³ and T_g (-132.5 °C)²⁴. Similarly, the 9.5 m H₃PO₄ ($T_e = -85 \text{ °C}$)²⁵ and 7.5 m ZnCl₂ ($T_e = -63 \text{ °C}$)²⁶ can support aqueous batteries to operate at -88 °C (ref. 27) and -90 °C (ref. 22), respectively, which are also attributed to the strong SCA of H₂O-H₃PO₄ and H₂O-ZnCl₂ systems. According to the non-equilibrium H₂O-solute phase diagram⁶, the lowest temperature at which an electrolyte can maintain a super-cooling liquid state is the T_g . The electrolytes in weakand strong-SCA H₂O-solute systems both have T_e and T_g , with T_g being much lower than Te. However, electrolytes in weak-SCA H2O-solute systems cannot support a battery to operate at temperatures below T_e because they will rapidly enter a crystalline state (which would therefore decrease the ionic conductivity) below T_e . In contrast, the electrolytes in strong-SCA H₂O-solute systems can maintain a super-cooling liquid state for a long time⁶ at temperatures between T_e and T_g , and they may still remain at a high enough ionic conductivity at temperatures above T_g , thus enabling a battery to operate at temperatures between T_e and T_g . Therefore, the T_g serves as the kinetic decisive temperature-limiting factor for low-temperature battery operation, and it is only applicable for batteries using a strong-SCA electrolyte. It is crucial to design anti-freezing electrolytes by choosing strong-SCA H₂O-solute systems for extremely low-temperature applications.

Here, in contrast to the traditional strategy that focuses on regulating $T_{\rm f}$, we focused on regulating $T_{\rm e}$ and SCA to design low- $T_{\rm e}$ and strong-SCA electrolytes for extremely low-temperature applications (Fig. 1). We discovered a general rule that H₂O-salt systems with high ionic-potential cations and H₂O-solvent systems with high solvent donor numbers usually have a strong SCA, according to many DSC experiments. Moreover, we proposed a general strategy whereby low-T_e and strong-SCA electrolytes can be realized by creating multiple-solute systems via introducing assisted salts with high ionic-potential cations (for example, Al³⁺, Ca²⁺) or cosolvents with high donor numbers (for example, ethylene glycol (EG)). As a demonstration in Na-based H_2O -solute systems, the designed low- T_e and strong-SCA1mNaCF₃SO₃ + 2.5 mAl(CF₃SO₃)₃ (Na-H₂O-Al), H₅₀EG₅₀-2 m NaCF₃SO₃ (Na-H₂O-EG) and 1 m NaClO₄ + 4 m Ca(ClO₄)₂ (Na-H₂O-Ca) electrolytes exhibit ultralow T_e (-53.5 to -72.6 °C) and T_g (-86.1 to -117.1 °C), with the low- T_e and strong-SCA mechanisms revealed to be related with electrolyte local structure coordination environments, H₂O-salt interactions, and complex competing ordering effects. The designed electrolytes enabled the superior performance of the $Na_{1.65}Fe_{0.21}Mn_{0.79}[Fe(CN)_6]_{0.92}$ ·2.08H₂O (NaFeMnHCF)/Na-H₂O-EG/ NaTi₂(PO₄)₃ full cell (80 Wh kg⁻¹ at 25 °C with 70% capacity retention over 5,000 cycles at 8 C, 63 Wh kg⁻¹ at -60 °C and 0.05 C) and the NaFeMnHCF/Na-H₂O-Ca/3,4,9,10-perylenetetracarboxylic diimide (PTCDI) full cell (65.7 Wh kg⁻¹ at 25 °C with 91.1% capacity retention over 250 cycles at 4 C, 20 Wh kg⁻¹ at -80 °C and 0.1 C, and 12.5 Wh kg⁻¹ at -85 °C and 0.1 C). This work marks an important development in

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Fig. 2 Design of low-T and strong-SCA aqueous electrolytes. a. The relationship of SCA attribute and cation ionic potential in various H₂O-salt systems. The weak-SCA and strong-SCA zones are identified by T_e heat-flow peak and T_{g} heat-flow step on the DSC heating curves, respectively. **b**, The relationship of SCA attribute and solvent donor number in various H₂O-solvent systems.

anti-freezing electrolyte designs for extremely low-temperature applications.

Design low-T_e and strong-SCA aqueous electrolytes

To develop an effective guideline for designing low-T_e and strong-SCA aqueous electrolytes, we first examined what kind of H₂O-solute systems will have strong SCA. From DSC heating curves (see Supplementary Note 1 and Supplementary Fig. 1a-c for the conventional DSC analysis method^{24,28,29}), one can observe a heat-flow signal of T_{a} or T_{a} for dilute solutions in an H₂O-solute system and identify its attribute (strong or weak) of SCA accordingly. The appearance of T_{e} heat-flow peak in an H₂O-solute system^{30,31} indicates the weak SCA due to the complete crystallization during cooling, whereas the appearance of T_{σ} heat-flow step^{24,32} indicates the strong SCA because of the dominant glass state rather than the crystalline state during cooling. Therefore, a criterion can be proposed to distinguish weak- and strong-SCA H₂Osolute systems based on DSC data at a fixed cooling-heating rate: a dilution solution showing a T_e heat-flow peak and a T_g heat-flow step in DSC curve belong to the weak- and strong-SCA H₂O-solute systems, respectively (see examples in Supplementary Fig. 2a-c).

Although SCA attributes of a large number of H₂O-solute systems (the solute could be salt or cosolvent) can be obtained based on DSC data from the literature^{24,31,32} and laboratory measurements (Supplementary Fig. 3a,b), there still lacks a guideline to directly design strong-SCA electrolytes through adjusting physicochemical parameters of H2O-solute systems. Here, we discover that the ionic potentials of cations in salts and the donor numbers of cosolvents have a strong correlation with the SCA attribute (Fig. 2a, b and Supplementary Tables 1 and 2). For H₂O-salt systems (Fig. 2a), it is found that with the fixed anion of CF₃SO₃, most salts with low ionic-potential cations

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Solvents used were ACN, sulfolane, propylene carbonate (PC), ethylene carbonate (EC), glycerol, EG and dimethylsulfoxide (DMSO). c, Schematic illustration of the proposed general strategy for designing low- T_e and strong-SCA electrolytes. d, The DSC heating curves of 4.5 m NaCF $_3$ SO $_3$ electrolytes, 1 m NaCF $_3$ SO $_3$ + 2.5 m $Al(CF_3SO_3)_3 (Na-H_2O-Al) and H_{50}EG_{50}-2 m NaCF_3SO_3 (Na-H_2O-EG) electrolytes.$

(for example, K^+ 7.25 e nm⁻¹) fall into the weak-SCA zone, while the $Al(CF_3SO_3)_3$ salt with high ionic-potential cation (Al^{3+} 56.07 e nm⁻¹) falls into the strong-SCA zone. Other salts with fixed anions (CI^{-} and NO_{3}^{-}) also obey a similar rule. For H₂O-solvent systems (Fig. 2b), it can be seen that solvents with low donor numbers, such as acetonitrile (ACN) (donor number 14.1), fall into the weak-SCA zone, whereas solvents with high donor numbers, such as the EG (donor number 20.0), fall into the strong-SCA zone. As a result, H₂O-salt systems with high ionic-potential cations and H₂O-solvent systems with high donor-number cosolvents are beneficial for systems falling into the strong-SCA zone.

In contrast to the SCA attribute that can be clearly correlated with the physicochemical parameters of H₂O-solute systems, it is difficult to find a similar rule for depicting the attribute (high or low) of T_e in H_2O -solute systems. Nevertheless, a low T_a can be realized by increasing the solute number because multiple-solute systems usually have lower $T_{\rm e}$ values than single-solute systems^{33,34}. Therefore, we can propose a general design strategy for realizing low- $T_{\rm e}$ and strong-SCA electrolytes, which involves creating multiple-solute systems via introducing salts with high ionic-potential cations or cosolvents with high donor numbers, as illustrated in Fig. 2c.

To demonstrate the efficacy of the strategy proposed above, we take the Na-based system as an example to design low- T_e and strong-SCA electrolytes. Owing to the relatively low ionic potential of Na⁺ (9.80 e nm⁻¹), most Na-based H₂O-salt electrolytes exhibit weak SCA, as demonstrated by the DSC data (Supplementary Fig. 4). The DSC results also show that most of Na-based H₂O-salt electrolytes have relatively high T_e (H₂O-Na₂SO₄ -1.2 °C, H₂O-NaCF₃SO₃ -20.5 °C, H₂O-NaClO₄-34.1 °C and so on). Both features limit the aqueous Na-ion batteries to operate at extremely low temperatures. Therefore, it is crucial to design low-Te and strong-SCA electrolytes for Na-based LTABs. Taking the H₂O-NaCF₃SO₃ system as an example, the DSC curves of



Fig. 3 | **The low-** T_{e} **mechanisms in designed electrolytes. a**, The fitted Raman spectra of H₂O, 4.5 m NaCF₃SO₃, Na-H₂O–Al and Na-H₂O–EG electrolytes from 2,500 to 4,000 cm⁻¹ at 25 °C. **b**, The calculated average H-bond numbers in H₂O, 4.5 m NaCF₃SO₃, Na-H₂O–Al and Na-H₂O–EG structures. **c**, The coordination species and numbers (cut-off radius 4 Å) around O_w atom in various structures.

both dilute 10 wt% NaCF₃SO₃ (Supplementary Fig. 4) and eutectic-point concentration 4.5 m NaCF₃SO₃ electrolytes (Fig. 2d) demonstrate the high- T_e (-20.5 °C) and weak-SCA properties. When introducing a weak-SCA-zone KCF₃SO₃ salt or ACN cosolvent (Supplementary Fig. 5a,b), all the obtained electrolytes exhibit crystal melting heat-flow peaks and have no T_{α} heat-flow step, demonstrating that they failed to realize strong SCA. In comparison, when introducing strong-SCA-zone Al(CF_3SO_3)₃ salt or EG cosolvent into the H₂O-NaCF₃SO₃ system, all the obtained electrolytes exhibit T_{σ} heat-flow steps (Fig. 2d and Supplementary Fig. 6a,b), demonstrating that they successfully realized strong SCA. It can be seen that the insufficient $Al(CF_3SO_3)_3$ salt or EG cosolvent results in cold crystallization heat-flow peak on the DSC heating curve, whereas an excess amount Al(CF₃SO₃)₃ salt or EG cosolvent leads to a high $T_{\rm g}$ value (Supplementary Fig. 6a,b). To ensure there is no cold crystallization and low T_g , 1 m NaCF₃SO₃ + 2.5 m Al(CF₃SO₃)₃ (Na-H₂O-Al; $T_g = -86.1 \text{ °C}$ and $H_{50}EG_{50}-2 \text{ m NaCF}_3SO_3 (\text{Na}-\text{H}_2\text{O}-\text{EG}; T_g = -114.5 \text{ °C})$ are chosen as electrolytes for Na-based LTABs. In addition, the T_e of Na-H₂O-Al and Na-H₂O-EG electrolytes is estimated as -53.5 and -67.5 °C (Supplementary Fig. 6a,b), respectively, both of which are much lower than that of the H_2O -NaCF₃SO₃ system (-20.5 °C). As a result, we have been able to successfully design low- T_e and strong-SCA electrolytes by creating multiple-solute systems via introducing the $AI(CF_3SO_3)_3$ salt with high ionic-potential cation (Al³⁺ ionic potential 56.07 e nm⁻¹) or the EG cosolvent with high donor number (EG donor number 20.0) into the high- T_e and weak-SCA H₂O-NaCF₃SO₃ system. In addition to the example demonstrated above, we have included more examples regarding the designs of anti-freezing electrolytes in Na-based systems (Supplementary Figs. 7a, b and 8a, b and Supplementary Note 2), such as $1 \text{ m NaClO}_4 + 4 \text{ m Ca(ClO}_4)_2 (\text{Na}-\text{H}_2\text{O}-\text{Ca}) (T_e = -72.6 \text{ °C}, T_g = -117.1 \text{ °C}),$ demonstrating the general applicability of the proposed strategy.

Mechanisms of low T_e and strong SCA in designed electrolytes

To clarify why low- T_e and strong-SCA electrolytes can be efficiently designed using our proposed strategy in Fig. 2c, we performed Raman scattering and nuclear magnetic resonance (NMR) spectroscopy analyses as well as ab initio molecular dynamic (AIMD) simulations and density functional theory (DFT) calculations to the designed electrolytes, especially for Na-H₂O-Al and Na-H₂O-EG electrolytes.

Regarding the low T_e , this is associated with high electrolyte entropy based on the thermodynamic theory⁶, namely a high degree of disorder in atomic coordination environment of electrolyte structures. The thermodynamic liquid-to-solid low-temperature limits are as follows: H₂O (0 °C) > 4.5 m NaCF₃SO₃ (-20.5 °C) > Na-H₂O-Al (about -53.5 °C) > Na-H₂O-EG (about -67.5 °C), indicating that the disorder of atomic coordination environment increases along the sequence. The mechanisms can be understood from two perspectives.

First, the degree of disorder of atomic coordination environment for different aqueous solutions can be reflected by the degree of hydrogen-bond (H-bond) breakage between water molecules, which can be studied by the OH stretching vibration (I_{OH}) bands between 3,000 and 4,000 cm⁻¹ on Raman spectra and the average H-bond numbers based on AIMD statistical analyses. In pure water, the I_{OH} band is usually analysed by the two-state model including the hydrogen-bonded scatterers and non-hydrogen-bonded scatterers^{35,36}. In aqueous solutions, the I_{OH} band can also be analysed by two factors including hydrogen-bonded scatterers and non-hydrogen-bonded (ion or solvent-hydrated) scatterers^{37,38}. Here we use two Gaussian peaks (weak vibration band I_w and strong vibration band I_s , representing the predominant contribution of hydrogen- and non-hydrogen-bonded scatterers, respectively) to fit the I_{OH} bands (for the fitting in Na-H₂O-EG system, the additional two Gaussian peaks are used to represent the C-H vibration band I_{CH} ; Fig. 3a) and define amplitude ratio (I_W/I_S) to reflect the degree of H-bond breakage (Fig. 3a). The order of I_w/I_s values is as follows: H₂O (0.72) > 4.5 m NaCF₃SO₃ (0.54) > Na-H₂O-Al (0.47) > Na-H₂O-EG (0.38), which is consistent with the order of liquid-to-solid low-temperature limits. Meanwhile, the AIMD results demonstrate that the average H-bond numbers between water molecules (Fig. 3b) show a similar order: $H_2O(3.4) > 4.5 \text{ m NaCF}_3SO_3$ $(2.8) > Na-H_2O-AI (2.4) > Na-H_2O-EG (1.9)$. A lower I_W/I_s value and a smaller average number of H-bonds indicate a higher degree of H-bond breakage and increased H-bond disorder within the electrolyte structure, which consequently leads to a lower liquid-to-solid low-temperature limit.

Second, the degree of disorder in different aqueous solutions can also be reflected by the coordination species and numbers around the O_w (oxygen atom in water) atoms. According to the AIMD simulation results (Fig. 3c, Supplementary Fig. 9a–f and Supplementary Table 3),



Fig. 4 | The strong-SCA mechanisms in designed electrolytes. a, Mean squared displacement (MSD) of the H atom at 300 K in 4.5 m NaCF₃SO₃ and Na-H₂O-Al electrolytes. b, The calculated average binding energy of H₂O molecules in 4.5 m NaCF₃SO₃ and Na-H₂O-Al electrolytes. H₂O-all, all H₂O molecules in electrolytes.

 H_2O -bond, H_2O molecules bonded with Na^{\ast} (H_2O-Na^{\ast}) or $Al^{3\ast}$ $(H_2O-Al^{3\ast})$ in a $Na-H_2O-Al$ electrolyte. c, Typical local structures for liquid electrolytes (4.5 m NaCF_3SO_3 and Na-H_2O-EG) and solid crystallization components (ice and NaCF_3SO_3 \cdot H_2O). The dotted line denotes the H-bond.

the pure H₂O has only two coordination species around the O_w atom $(O_w - H_w)$ (hydrogen atom in water) and $O_w - O_w$) with respective coordination numbers of 19.5 and 7.4 in a cut-off radius of 4 Å. In comparison to pure H₂O, O_w atoms in 4.5 m NaCF₃SO₃ structure not only exhibit different coordination numbers (15.4 and 6.7) for the ordinary coordination species (O_w-H_w and O_w-O_w), but also show two new coordination species (O_W -Na and O_W - O_{OTF} (oxygen atom in a CF₃SO₃ anion)) with coordination numbers of 0.6 and 1.2, respectively. Regarding the Na-H₂O-Al and Na-H₂O-EG electrolytes, the above-mentioned $O_w - H_w$, $O_w - O_w$, $O_w - Na$ and $O_w - O_{OTF}$ coordination species also exist but with different coordination numbers (Supplementary Table 3). Also, new species of O_W -Al (coordination number 0.3) and O_W - O_{FG} (oxygen atom in an EG molecule) (coordination number 1.8) appear, respectively (Supplementary Table 3). Therefore, the designed Na-H₂O-Al and Na-H₂O-EG electrolytes have more complex and diverse atomic coordination environments than the 4.5 m NaCF₃SO₃ electrolyte, thus resulting in a degree of higher disorder and lower T_{e} .

Regarding the strong SCA, this is associated with a strong frustration against crystallization process at low temperatures³⁹, which involves strong H₂O-solute interaction and a complex competing ordering effect, with the latter being a well-known mechanism in the field of metallic glasses^{40,41}. The strong-SCA mechanisms of Na–H₂O–Al and Na–H₂O–EG electrolytes should be understood from different perspectives because salt and cosolvent have different properties. We revealed that the H₂O–salt interaction plays a dominant role in electrolytes containing high-ion-potential cations, whereas the complex competing ordering effect plays a dominant role in electrolytes containing high donor-number cosolvents.

For the Na-H₂O-Al electrolyte, its strong-SCA mechanism can be interpreted by examining H₂O-solute interactions and the water diffusion kinetics using AIMD simulations, DFT calculations and two-dimensional diffusion-ordered NMR spectroscopy (2D-DOSY-NMR). As shown in Fig. 4a, the mean squared displacement of Hatomin the Na-H₂O-Al electrolyte is much lower than that in the 4.5 m NaCF₂SO₃ electrolyte within 40 ps. indicating slower water diffusion kinetics in the Na-H₂O-Al electrolyte. The 2D-DOSY-NMR results (see the ¹H NMR spectra in Supplementary Fig. 10) further demonstrated that the Na-H₂O-Al electrolyte has a lower ¹H diffusion coefficient $(4.1 \times 10^{-10} \text{ m}^2 \text{ s}^{-1})$ than the 4.5 m NaCF₃SO₃ electrolyte $(6.4 \times 10^{-10} \text{ m}^2 \text{ s}^{-1})$. This should be attributed to different H₂O-solute interactions in both electrolytes, which can be revealed by DFT calculations. As shown in Fig. 4b, the calculated average binding energy of H₂O molecules in Na-H₂O-Al (1.37 eV) is higher than that of 4.5 m NaCF₃SO₃ (1.13 eV), which should be responsible for the lower ¹H diffusion coefficient in the Na-H₂O-Al electrolyte. A higher average binding energy means that local atomic rearrangement for ice precipitation during the crystallization process is more difficult, thus resulting in a stronger SCA. We believe that after introducing Al(CF₃SO₃)₃ salt into an H₂O-NaCF₃SO₃ system, the increased average binding energy should be attributed to the higher ionic potential of AI^{3+} (56.07 e nm⁻¹) than Na⁺ (9.80 e nm⁻¹). This can be demonstrated by the higher average binding energy of H_2O molecules bonded with Al^{3+} (2.48 eV of H_2O-Al^{3+}) than that of H_2O molecules bonded with Na⁺ (1.41 eV of H₂O-Na⁺) in the Na-H₂O-Al electrolyte (Fig. 4b). In contrast, after introducing KCF₃SO₃ salt with a low ionic potential of K⁺ (7.25 e nm⁻¹) into the H₂O-NaCF₃SO₃ system, the obtained 1 m NaCF₃SO₃ + 2.5 m KCF₃SO₃ (Na-H₂O-K) electrolyte

still has a weak SCA, which is attributed to a low H_2O molecule average binding energy (Supplementary Fig. 11 and Supplementary Note 3). These insights clarified why introducing a salt with high ionic-potential cation into the weak-SCA H_2O -NaCF₃SO₃ system can realize strong SCA.

For the Na-H₂O-EG electrolyte, its strong SCA can be understood by the complex competing ordering effect, which stems from local structure differences between liquid electrolyte and solid crystallization components^{40,41}. AIMD simulations are adopted to examine the local structures with the assumption that both 4.5 m NaCF₃SO₃ and Na-H₂O-EG electrolytes would form the solid crystallization components containing ice and monohydrate NaCF₃SO₃·H₂O crystals during the cooling process. Typical atomic-level local structures are extracted from the AIMD snapshots of 4.5 m NaCF₃SO₃ and Na-H₂O-EG electrolyte models as well as the experimental structures of ice and NaCF₂SO₂·H₂O crystals (Fig. 4c and Supplementary Fig. 12a-d). The H-bond local structure difference between the Na-H2O-EG electrolyte (diverse H-bond coordinating structures between H2O and EG molecules) and ice crystal (four H-bond coordinating structures) is more noticeable than the difference between the 4.5 m NaCF₃SO₃ electrolyte (two or three H-bond coordinating structures) and ice crystal. Similarly, the Na-H₂O-EG electrolyte also exhibits a greater Na-coordination local structure difference (Na-3O_w-2O_{EG} and Na-O_{OTF}-2O_w-2O_{EG}) to the NaCF₃SO₃·H₂O crystal (Na-2O_w-4O_{OTF}) than that of the 4.5 m NaCF₃SO₃ electrolyte $(Na-5O_w and Na-4O_w-O_{OTF})$ to the NaCF₃SO₃·H₂O crystal. The greater the disparity in local structure between liquid electrolytes and solid crystallization components, the longer the atomic diffusion distance during the electrolyte crystallization process³⁹, thus frustrating the crystallization and resulting in a stronger SCA. The remarkably increased local structure difference between designed electrolyte and solid crystallization components after introducing the EG solvent into the H₂O-NaCF₃SO₃ system should be attributed to the high donor number (20.0) of the EG solvent, which is beneficial for coordinating with H₂O and Na⁺. In contrast, after introducing the low donor-number (14.1) ACN cosolvent into the H₂O-NaCF₃SO₃ system, the obtained H₅₀ACN₅₀-2 m NaCF₃SO₃ (Na-H₂O-ACN) electrolyte still has a weak SCA, which should be attributed to the weak coordinating ability of the ACN molecule with H₂O and Na⁺ (Supplementary Fig. 13 and Supplementary Note 3). These insights clarified why adding a high donor-number cosolvent into the weak-SCA H₂O-NaCF₃SO₃ system can result in a strong SCA.

In short, the mechanisms of low- T_e and strong-SCA properties are mainly associated with the local structure coordination environment, H₂O-salt interactions and complex competing ordering effects. The introduced assisted salts or cosolvents can increase electrolyte entropy by breaking H-bonds and enriching local structure coordination species, thus realizing low T_e . The assisted salts with high cation ionic potentials can enhance the H₂O-solute interaction, whereas the cosolvents with high donor numbers can increase local structure difference between the liquid electrolyte and solid crystallization components, both of which lead to strong frustration against crystallization process at low temperatures, thus realizing a strong SCA. These insights rationalize the low T_e and strong SCA of designed electrolytes as well as the proposed general design strategy for anti-freezing electrolytes in Fig. 2c.

Battery demonstrations for designed electrolytes

To show battery performance using the designed electrolytes at various temperatures, we synthesized the Prussian blue analogous cathode NaFeMnHCF (chemical formula $Na_{1.65}Fe_{0.21}Mn_{0.79}[Fe(CN)_6]_{0.92}$ ·2.08H₂O) and prepared two anode materials: a polyanionic anode NaTi₂(PO₄)₃ for achieving high energy density and an organic anode PTCDI for realizing ultralow temperature operation. The structural and compositional characterizations of electrode materials are depicted in Supplementary Figs. 14–17, Supplementary Tables 4 and 5 and Supplementary Note 4.

We examined the performance of NaFeMnHCF//NaTi₂(PO₄)₃ full cells in various electrolytes and temperatures. For full cells using the weak-SCA 4.5 m NaCF₃SO₃, Na-H₂O-K and Na-H₂O-ACN electrolytes,

the lowest operating temperatures are not lower than the T_e of these electrolytes, which are -20.5, -26.3 and -53.1 °C, respectively (Supplementary Fig. 18a-c). Since the weak-SCA electrolytes would rapidly become crystalline at temperatures below their T_e , the ion diffusions in these electrolytes are completely prevented. In contrast, benefiting from low T_e and strong SCA, both Na-H₂O-Al (T_e = -53.5 °C, T_g = -86.1 °C) and Na-H₂O-EG (T_e = -67.5 °C, T_g = -114.5 °C) electrolytes have high enough ionic conductivities at ultralow temperatures (Supplementary Table 6), enabling the NaFeMnHCF//NaTi₂(PO₄)₃ full cells to deliver reversible capacities at temperatures from -60 to 25 °C and even light bulbs at -70 °C (Fig. 5a-c and Supplementary Fig. 18d).

The NaFeMnHCF//NaTi₂(PO₄)₃ full cells using the Na-H₂O-EG electrolyte exhibited a much better performance than those using the Na-H₂O-Al electrolyte. In the Na-H₂O-Al electrolyte, the full cells show limited lifespans at -60 to 25 °C (4-14 cycles) (Supplementary Fig. 19a), which are much lower than full cells in the Na-H₂O-EG electrolyte (27-5,000 cycles) (Fig. 5a-c). The full cells using the Na-H₂O-Al electrolyte have issues of Al3+-ion insertion on the cathode side (Supplementary Fig. 19b) and severe H₂ evolution on the anode side (the Na-H₂O-Al electrolyte pH value is roughly 4), whereas full cells using the Na-H₂O-EG electrolyte do not exhibit these issues. In addition, the Na-H₂O-EG electrolyte has lower T_e and T_g , wider voltage window and higher low-temperature ionic conductivity than the Na-H₂O-Al electrolyte (Supplementary Fig. 20a, b and Supplementary Table 6). Therefore, we focused on the performance of NaFeMnHCF//NaTi₂(PO₄)₃ full cells using the Na-H₂O-EG electrolyte at various temperatures. At 25 °C, the NaFeMnHCF/Na-H₂O-EG/NaTi₂(PO₄)₃ full cell delivers an energy density of 80 Wh kg⁻¹ at 2 C, maintains 88% capacity retention from 2 to 10 C and exhibits 70% capacity retention at 8 C over 5,000 cycles (Fig. 5c and Supplementary Fig. 21a). At -40 °C, the full cell delivers an energy density of 72 Wh kg⁻¹ at 0.1 C, maintains 68% capacity retention from 0.1 to 0.5 C and shows 96% capacity retention after 80 cycles at 0.5 C (Supplementary Fig. 21b,c). At -60 °C, the full cell delivers an energy density of 63 Wh kg⁻¹ at 0.05 C and maintains 65% capacity retention from 0.05 to 0.15 C (Fig. 5b and Supplementary Fig. 21d).

To demonstrate an aqueous Na-ion battery with a more impressive low-temperature performance, we assembled the NaFeMnHCF// PTCDI full cell using the designed Na-H₂O-Ca electrolyte ($T_e = -72.6$ °C, $T_{\rm g}$ = -117.1 °C). Benefiting from the high ionic conductivity of the electrolyte (112.5 mS cm⁻¹ at 25 °C, 0.8 mS cm⁻¹ at -80 °C; Supplementary Table 6), the NaFeMnHCF/Na-H₂O-Ca/PTCDI full cell can stably operate at temperatures ranging from 25 to -85 °C. We examined the performance of both coin and pouch cells at various temperatures (Fig. 5d,e and Supplementary Figs. 22a-d and 23a-c). At 25 °C, the coin cell delivers a high energy density of 65.7 Wh $kg^{\mbox{--}1}$ and remains at 91.1% capacity retention over 250 cycles at 4 C (Supplementary Fig. 22a,b). At -60 °C, the coin cell delivers a high energy density of 46.3 Wh kg⁻¹ and remains at 85.1% capacity retention over 70 cycles at 0.5 C (Supplementary Fig. 22c,d). At -80 °C, the coin cell delivers a high energy density of 20 Wh kg⁻¹ and remains at 93.1% capacity retention over 20 cycles at 0.1 C (Fig. 5e and Supplementary Fig. 23a). At -85 °C, the coin cell delivers an energy density of 12.5 Wh kg⁻¹ at 0.1 C (Supplementary Fig. 23b). As shown in Fig. 5d and Supplementary Fig. 23c, the assembled pouch cell delivers 10.4, 6.9, 4.9 and 2.3 mAh at 25, -60, -80 and -85 °C, respectively. Compared with reported aqueous Na-ion batteries^{13,15,42-46} (Supplementary Fig. 24 and Supplementary Table 7), our demonstrated full cells achieve the best overall performance in terms of energy density, cycling lifespan and lower limit of operating temperature.

Conclusions

In summary, we recognized two liquid-to-solid low-temperature limits (T_e and T_g) of H₂O-solute systems, as well as the importance of designing anti-freezing electrolytes by choosing low- T_e and strong-SCA H₂O-solute systems for extremely low-temperature applications. We proposed a general strategy that low- T_e and strong-SCA electrolytes can be realized



Fig. 5 | Battery demonstrations in designed electrolytes. a, The discharge curves of the NaFeMnHCF/Na-H₂O-EG/NaTi₂(PO₄)₃ full cell at various temperatures. The inset photograph shows the bulbs lighted by full cells at -70 °C. b,c, Rate capability and cycling stability of the NaFeMnHCF/Na-H₂O-EG/

 $NaTi_2(PO_4)_3 \text{ full cell at } -60 \ ^\circ \text{C} (\textbf{b}) \text{ and } 25 \ ^\circ \text{C} (\textbf{c}). \textbf{d}, \text{Typical discharge curves of} \\ NaFeMnHCF/Na-H_2O-Ca/PCDI \text{ pouch cell at temperatures ranging from } -85 \text{ to} \\ 25 \ ^\circ \text{C}. \text{ The inset is a photograph of the assembled pouch cell. } \textbf{e}, \text{ Cycling stability} \\ \text{of a NaFeMnHCF/Na-H_2O-Ca/PCDI coin cell at } -80 \ ^\circ \text{C} \text{ and } 0.1 \ \text{C}. \\ \end{cases}$

by creating multiple-solute systems via introducing assisted salts with high ionic-potential cations or cosolvents with high donor numbers. Taking the Na-based system as an example, the designed low- T_e and strong-SCA Na-H₂O-Al, Na-H₂O-EG and Na-H₂O-Ca electrolytes show ultralow T_e (-53.5 to -72.6 °C) and T_g (-86.1 to -117.1 °C), enabling the superior performance of the NaFeMnHCF/Na-H₂O-EG/NaTi₂(PO₄)₃ full cell (80 Wh kg⁻¹ at 25 °C with 70% capacity retention over 5,000 cycles at 8 C, 63 Wh kg⁻¹ at -60 °C and 0.05 C) and the NaFeMnHCF/Na-H₂O-Ca/PTCDI full cell (65.7 Wh kg⁻¹ at 25 °C with 91.1% capacity retention over 250 cycles at 4 C, 20 Wh kg⁻¹ at -80 °C and 0.1 C, 12.5 Wh kg⁻¹ at -85 °C and 0.1 C). The mechanisms of low- T_e and strong-SCA properties are revealed to be associated with local structure coordination environment, H₂O-salt interaction and a complex competing ordering effect. This work provides an effective guideline for anti-freezing electrolyte designs, marking an important development for extreme LTABs.

Methods

Materials and electrolytes

The NaFeMnHCF cathode was prepared by a simple precipitation method. Typically, 2 mmol Na $_4$ Fe(CN) $_6$ ·10H $_2$ O and a corresponding

proportion of FeSO₄·7H₂O (0.4 mmol) and MnSO₄·H₂O (1.6 mmol) were dissolved into 100 and 80 ml of H₂O–EG hybrid solution (equal volume), respectively. Then, the latter solution was slowly dropped into the former with magnetic stirring at room temperature. After 12 h, the precipitate formed was centrifuged and washed thoroughly with deionized water. The final product was obtained after drying in air under 80 °C for 12 h. The NaTi₂(PO₄)₃ was synthesized through the sol-gel method according to the literature⁴⁷. The PTCDI powder (CAS number 81–33–4) was purchased from TCI Co., Ltd. The H_xEG_y·2 m NaCF₃SO₃ electrolyte was made by dissolving the 2 mmol NaCF₃SO₃ in 2 g of solvent (prepared by x% ml of H₂O and y% ml of EG). The 1 m NaCF₃SO₃ + 2.5 m Al(CF₃SO₃)₃ electrolyte was obtained by dissolving the 1 mmol NaCF₃SO₃ and 2.5 mmol Al(CF₃SO₃)₃ in 1 g H₂O. Other electrolytes were prepared in a similar way to the H_xEG_y·2 m NaCF₃SO₃ + 2.5 m Al(CF₃SO₃)₃ electrolytes.

Electrochemical measurements

The NaFeMnHCF and NaTi₂(PO₄)₃ electrodes were fabricated using active materials, carbon black and polytetrafluorothylene at a weight ratio of 7/2/1. The CR2032-type coin cells are used to assemble the

NaCF₃SO₃, two Al(CF₃SO₃)₃ and 55 H₂O within a 13.5 \times 13.5 \times 13.5 Å³ cubic

supercell. The Na-H₂O-EG electrolyte calculation model contained

two NaCF₃SO₃, nine (CH₂OH)₂ and 28 H₂O within a 13.0 \times 13.0 \times 13.0 Å³

cubic supercell. The Na-H₂O-K electrolyte calculation model con-

tained one NaCF₃SO₃, two KCF₃SO₃ and 55 H₂O within a

 $13.0 \times 13.0 \times 13.0$ Å³ cubic supercell. The Na-H₂O-ACN electrolyte

calculation model contained two NaCF₃SO₃, ten CH₃CN and 31 H₂O

within a 13.0 × 13.0 × 13.0 Å³ cubic supercell. All initial electrolyte struc-

tures of calculation models were constructed using the Packmol soft-

ware⁵⁵ according to the experimental density. The ice (mp-697111) and

NaCF₃SO₃·H₂O (mp-601202) crystal structures comes from the website

https://materialsproject.org/. The average binding energy of the H₂O

molecule was calculated using DFT based on the structure of the AIMD

snapshot. The binding energy of an H₂O molecule in electrolyte is

calculated by the formula as follows: $E_{\rm b} = E_{\rm H_2O} + E_{\rm electrolyte}^1 - E_{\rm electrolyte}^0$, where the $E_{\rm b}$ is the binding energy of the H₂O molecule in electrolytes,

 $E_{\rm H_2O}$ is energy of the H₂O molecule in a vacuum, $E^{\rm O}_{\rm electrolyte}$ is energy of

the electrolyte structure model obtained by AIMD simulation and

NaFeMnHCF/Na-H₂O-EG/NaTi₂(PO₄)₃ and NaFeMnHCF/Na-H₂O-Ca/PTCDI full cells (cathode/anode mass ratio was 1/0.9). The Swagelok-type cells (Ti foil was used to protect against proton corrosion) NaFeMnHCF/Na-H₂O-Al/NaTi₂(PO₄)₃ full cell (cathode/anode mass ratio was 1/1.5). The mass loading values for NaFeMnHCF and NaTi₂(PO₄)₃, and PTCDI electrodes in coin cells were about 5.2 and 4.1 mg cm⁻², respectively. The mass loading values for NaFeMnHCF and PTCDI electrodes in pouch cells were about 12.4 and 10.6 mg cm⁻², respectively. The reversible capacities of NaFeMnHCF/Na-H₂O-EG/ $NaTi_{2}(PO_{4})_{3}$ and $NaFeMnHCF/Na-H_{2}O-Ca/PTCDI full cells are shown on$ the basis of cathode mass, whereas the reversible capacity of NaFeMn- $HCF/Na-H_2O-Al/NaTi_2(PO_4)_3$ full cell is displayed on the basis of anode mass. The energy densities of all full cells were calculated by total active mass of cathode and anode. All charge-discharge curves were performed using the NEWARE Battery Test System (catalogue no. CT-4008-5V50mA-164).

Material characterizations

DSC tests were carried out in DSC200F3 at a temperature range from 25 to -150 °C. All samples had mesophase carbon micro-beads added to promote nucleation⁴⁸. The cooling-heating rates were 20 K min⁻¹ (to keep to the same testing conditions of Cl-based and NO₃-based H_2O -salt systems in the literature²⁴) for 10 wt% LiNO₃ and 10 wt% KCl aqueous solution samples. The cooling-heating rates of other samples were 10 K min⁻¹. The Raman spectroscopy for the electrolyte OH stretch was conducted on a HORIBA HR Evolution microscope using a 532 nm excitation laser. The ¹H 2D-DOSY-NMR spectra were produced using a Bruker DRX 600 spectrometer. The structures were characterized using an X'Pert Pro MPD X-ray diffractometer (D8 Bruker) with Cu K_{α} radiation ($\lambda = 1.5405$ Å). X-ray photoelectron spectra were recorded with a spectrometer that had Mg/Al Ka radiation (ESCALAB 250 Xi, ThermoFisher). The morphologies of the electrodes were obtained by scanning electron microscopy (Hitachi-S4800). The thermogravimetric analysis for NaFeMnHCF cathode was conducted on a NETZSCH-STA449C thermal analysis device. The elemental ratios of Na, Fe and Mn in the NaFeMnHCF cathode were determined by inductively coupled plasma atomic emission spectrometry. For low-temperature tests, the cell performance was measured in ShangHai BoYi (B-T-107D and B-T-80-E) low-temperature ovens at temperatures ranging from -85 to 25 °C. The reference electrode for testing the electrochemical window at various temperatures was a Zn^{2+}/Zn electrode with 7.5 m ZnCl₂ electrolyte (-0.67 V versus a standard hydrogen electrode). Three NaFeMnHC/Na-H₂O-EG/NaTi₂(PO₄)₃ coin cells (fully charged at room temperature) were used to power light emitting diode bulbs at -70 °C. The ionic conductivities of electrolytes were measured via an electrochemical impedance spectrum using the Pt electrode equipment purchased from Shanghai Russell Technology Co., Ltd. The linear sweep voltammetry experiments were conducted using a VMP3 electrochemical testing unit (BioLogic).

Computations

The DFT calculations were carried out by using the Vienna ab initio simulation package⁴⁹. The projector augmented-wave potentials⁵⁰ generated with Perdew–Burke–Ernzerhof generalized gradient approximation⁵¹ were used. The van der Waals interaction was taken into account by using the rev-vdWDF2 functional⁵². The plane wave cut-off energy was set to 400 eV and the Γ point was used for the Brillouin zone sampling. The AIMD simulations were performed in a canonical ensemble (NVT) by using a Nosé thermostat^{53,54}, with a time step of 1 fs. All molecular dynamics simulations were run for 40 ps at 400 K first, then run for 20 ps at 300 K to yield the data for analysis. The water calculation model contained 55 H₂O molecules within a 11.8 × 11.8 × 11.8 Å³ cubic supercell. The 4.5 m NaCF₃SO₃ electrolyte calculation model contained two NaCF₃SO₃ and 25 H₂O within a 10 × 10 × 10 Å³ cubic supercell. The Na–H₂O–Al electrolyte calculation model contained one

 $E^{1}_{electrolyte}$ is energy of the calculation model whose water numbers are one less than the electrolyte model obtained by AIMD simulation. The average H-bond numbers were calculated on the basis of the geometrical criterion of O-H…O angle <30° and the distance of two O being less than 0.35 nm. **Data availability** The datasets analysed and generated during the current study are included in the paper and its Supplementary Information. References 1. Xu, J. et al. Electrolyte design for Li-ion batteries under extreme operating conditions. Nature 614, 694-700 (2023). 2. Rodrigues, M.-T. F. et al. A materials perspective on Li-ion batteries at extreme temperatures. Nat. Energy 2, 17108 (2017). 3. Zhu, G. et al. Rechargeable Na/Cl₂ and Li/Cl₂ batteries. Nature 596, 525-530 (2021). 4. Ai, F. et al. Heteropoly acid negolytes for high-power-density aqueous redox flow batteries at low temperatures. Nat. Energy 7, 417-426 (2022).

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Author contributions

L.J., Y.-S.H., J.Z., Y.-C.L. and Y.L. conceived the project. L.J. synthesized the NaFeMnHCF cathode and carried out electrochemical tests, DSC tests, AIMD simulations and DFT calculations. S.H. synthesized the NaTi₂(PO₄)₃ anode and carried out NMR and DSC tests. Y.-C.H. contributed to the electrolyte strong-SCA mechanisms. L.J., S.H., Y.-C.H., Y.L, Y.-C.L., J.Z. and Y.-S.H. wrote the paper. All the authors participated in the preparation of paper.

Competing interests

Y.-S.H. is employed by HiNa Battery Technology Co., Ltd. The other authors declare no competing interests.

Additional information

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